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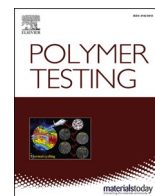
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Biogas upgrading with novel cellulose nano-crystals and polyvinyl amine nanocomposite membranes

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ABSTRACT

A novel crystalline nano cellulose (CNC) and polyvinyl amine (PVAm) based nanocomposite membranes were synthesized and evaluated for biogas upgrading. Different concentrations of CNC was incorporated in 3 wt % PVAm solution on commercial polysulfone (PSf) sheet using dip coating method. The effect of feed pressure (5, 10 and 15 bar) was investigated for the CO₂/CH₄ separation. The incorporation of CNC increased the crystallinity of membranes. The thickness of selective layer enhanced to 2.16 μm from 1.5 μm with increasing concentration of CNC. However, degree of swelling reduced from 75.88% to 68.93 with CNC concentration at 1.5 wt%. The best results were shown by PVAm membrane with 1 wt % CNC concentration i.e. CO₂ permeance of 0.0216 m³(STP)/m².bar.hr and selectivity (CO₂/CH₄) of 41. The permeance decreased approximately 1.8 folds for PVAm/1CNC membrane with the increase in pressure from 5 to 15 bar. However, selectivity dropped from 41 to 39 for formulated membranes.

1. Introduction

Reduction in Greenhouse gas (GHG) emission is driving the global concerns due to its profound impacts on our climate. Carbon dioxide (CO₂) a primary greenhouse gas, is mainly produced by burning of fuels and is estimated that the amount of CO₂ will increased to 37 Gt by 2035 [1]. Currently, 80% of world's energy demands are fulfilled by fossil fuels. If we follow the same trend, fossil fuels reservoirs will be consumed in approximately the next 100 years [2]. Furthermore, in order to limit global warming, it is required that energy use would have to be totally decarbonizes and renewable must provide 65% of global energy demands by 2050 [3]. Therefore, it is necessary to find the sustainable and renewable energy resources with low carbon emission. Currently, 18.6% of total world's energy demands are being fulfilled by renewable energy sources. However, bioenergy accounts for approximately 14% [4]. Hence, bioenergy would be expected to the most potential and sustainable source of renewable energy for future global primary energy mix in 2050 [5].

Biogas is a form of bioenergy and product of Anaerobic Digestion (decomposition in an oxygen deficient environment) of organic waste. It is mainly comprising of CH₄ (50–70) % and CO₂ (30–50) %. The relative concentration of these two gases largely depends on nature of raw

material and pH of bioreactor [6]. Biogas is being used for heating, production of steam and generation of electricity. However, after improving energy contents it can also be used as fuel for vehicles and grid stations. Presences of CO₂, mainly reduces the calorific value of biogas and limit its utilization. Upgraded biogas is also called as bio methane (>95% CH₄ contents) and can meet the technical requirements to replace the natural gas. Furthermore, the bio methane fuel has potential to reduce the non-methane volatile organic compounds emission by 50% and NO_x emissions by 25%. Furthermore, a significant reduction in particulate emission [7].

Biogas is upgraded by various techniques such as; water or amine scrubbing, pressure swing adsorption, membrane technology, and absorption [2]. The membrane separation is a proven green technology with cost effective CO₂ capture solution, and reduced footprints. Membrane technology has also been proven beneficial for low gas volumes and high CO₂ contents [8]. Therefore, membrane technology is highly recommended for the biogas upgrading by CO₂ removal [9]. Various strategies have been employed in past to manufacture polymeric membrane with high efficiency, cost effectiveness and ease of fabrication. However, due to transport mechanism mainly based molecular sieving and kinetic diameter, the inherent trade-off between selectivity and permeability of polymeric membranes is a challenge. Therefore, to

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overcome this limitation, Facilitated Transport Membranes (FTM) were first introduced as Supported Liquid Membranes (SLM). The moveable carriers react with dissolved CO₂. This complex is then transported across the membrane by solution diffusion mechanism. However, leakage of carrier in permeate and loss of solution by evaporation reduced the membrane performance with time. To overcome this problem, a new class of membranes has been evolved known as Fixed Site Carrier (FSC) membranes [10,11]. In FSC, the carrier is covalently bounded to the main polymer matrix. However, it reduced the free mobility of carrier but enhanced the overall stability and performance of membranes. Recently, research has been focused to make membrane material more hydrophilic to take the advantage of liquid membranes in highly swollen conditions [12–15]. The FTM that works under highly swollen conditions facilitate the CO₂ transport as bicarbonate ion (HCO₃⁻) through the membrane [16]. Utilization of such membranes have been reported in the literature and is revealed from the results that the degree of swelling is directly related to membrane performance [15, 17,18]. Furthermore, number of nano filler and carrier molecules has been incorporated to enhanced swelling as well as affinity of composite membranes for CO₂ [13,19].

Among different polymers used for acid gas separation, the polyvinyl amine is the most promising one. Due to the presence of abundant amine group and high degree of hydrophilicity, it gives high permeability and selectivity for CO₂. Furthermore, PVAm is easily soluble in the water at room temperature [10,20]. PVAm has been extensively investigated for CO₂ separation applications alone or with different combinations of fillers in mixed matrix membranes [10,12,21,22]. The structure of PVAm consists of amine group in its chain (-NH₂) which has a natural affinity for CO₂. It acts as fixed site carriers and facilitate transport of CO₂ across the membrane. Recently, Zhao et al. has used PVAm in mixed matrix composite membranes with PANI/PS and results showed that the presence of PANI nanoparticles in PVAm matrix enhanced separation performance of composite membranes [23]. Further, Ming Wang and Zhi Wang et al. incorporated inorganic fillers such as MWCNT, SiO₂ and ZSM-5 and study their interfacial properties. The study suggested that addition of nanofillers to PVAm matrix is an effective way to improve interfacial properties. However, better results could be obtained if inorganic filler and polymer has same functional groups [22]. But, stability issues of PVAm particularly at high pressure can be overcome by using high molecular weight PVAm or by introducing finely dispersed second phase in polymer matrix with high mechanical strength.

The Crystalline Nano cellulose (CNC) has been used in this research due to its high affinity with water and reinforcing nature [13,24–27]. Cellulose fibers have hierarchical microstructures and on acid hydrolysis give nanostructure of highly crystalline regions (CNC) and amorphous regions (CNF) [13,28–30]. D-glucopyranose (C₆H₁₁O₅) is a major component associated by β (1,4) links which is the repeating unit of cellulose [31]. The degree of polymerization of cellulose is difficult to determine but is reported to be near 10,000 if the molecular weight is around 3.2×10^6 g/mol. CNCs have become the center of attention for researchers due to its unique properties that include outstanding mechanical attributes, reinforcing capabilities, low density, biodegradability and excellent surface area per unit mass [13,18,24,28]. Moreover, cellulose is being abundantly used in bio and nano-composites. Due to biodegradable nature, cellulose has replaced multiple synthetic fibers which also contribute in polluting environment. Cellulose is also being used as nonstructural biocomposite in doors, windows, ceiling tiles etc. [32]. Recently, CNCs have been reported as an additive with PVA and showed enhanced results of CO₂ separation up to 15 bars. Furthermore, NFC has also been reported for enhanced performance of composite membranes. CNCs disperse along the polymeric matrix and help in moisture uptake and promotes swelling. This moisture content helps to increase the rate of facilitated transport of CO₂ across the membrane [18]. Furthermore, PVA has also been chemically cross-linked with CNCs resulting in excellent thermal stability and reinforcement capability. Cross-linked PVA/CNCs have also been

utilized in biocompatible electronic skin sensor system [33,34].

Thermodynamic properties of polymers play a vital role in the separation performance of membranes. Flory-Huggins theory describes the thermodynamics of polymer solutions and blends. It is a lattice model that explains the non-ideality of polymer mixtures. Comprehensive thermodynamic studies of polymeric blends have been carried out by Rana et al. for example, polyvinyl esters and polyacrylates, polystyrene-co-acrylonitrile and polyphenyl acrylate etc. Hydrogenated polymers were used as analogues of respective polymers and interaction energy densities were calculated [35–37]. However, in this work, polysulfone (PSf) and PVAm does not form blend and are chemically inert. Therefore, thermodynamics of these polymers have not been covered in this work.

This research work is carried out to improve the mechanical properties and water affinity of PVAm membranes to enhance CO₂ separation at moderately high pressures. CNC has been incorporated in PVAm matrix in order to get beneficial results. There has been no chemical crosslinking between PVAm and CNC. The membranes were investigated for the optimized concentration of CNC in 3% PVAm solution. Effect of addition of different concentrations of CNC on degree of swelling was investigated. The SEM analysis of membranes was conducted to find the effect of incorporation of CNC on morphology and thickness of selective layer. The effect on degree of crystallinity of PVAm/CNC nanocomposite membranes was investigated using XRD. The membrane rig used for CO₂ permeation testing was specially designed and has ability to work under humid conditions at moderately high pressure. Membranes were investigated under highly swollen conditions at 5, 10 and 15 bars. The results will be interpreted in terms of permeance of CO₂ and CH₄ and selectivity of CO₂/CH₄.

2. Experimental

2.1. Materials

Ultrafiltration flat sheet membrane of Polysulfone (PSf) (Molecular weight cut-off 50,000) of the commercial grade was purchased from Alfa Laval. CNCs were acquired from Cellulose Lab, Canada. The average width and length of CNC was 12 nm and 170 nm, respectively. Polyvinyl amine (MW 17,000–20,000) was purchased from Sigma Scientific. The solvent used for casting of membranes was deionized water.

2.2. Preparation of composite membrane

PVAm was added to deionized water and stirred for 3 h to get 3 wt % solution of polyvinyl amine. The mixture was left for rolling on mechanical roller overnight to obtain a clear solution. This procedure was carried out at room temperature. Afterwards, CNCs were added to the clear solution [38].

Different concentrations of CNCs with respect to weight percent of polymer i.e. 0.5%, 1% and 1.5%, were added to get casting solutions as shown in Table 1. The solutions were mechanically stirred overnight and sonicated afterwards for 30 min. The air bubbles should be removed from resultant suspension to cast defect free membranes. Therefore, solution was left at room temperature for 2 h. Using a dip-coating technique, a selective and dense membrane was casted on PSf sheet as shown in Fig. 1. The membranes were placed in fume hood overnight at room temperature for drying [10].

Table 1
Composition of casted membranes with their codes.

Membrane code	PVAm wt. %	Wt./Wt. CNC
Pure PVAm	3 g	–
PVAm/0.5CNC	3 g	0.5%
PVAm/1CNC	3 g	1%
PVAm/1.5CNC	3 g	1.5%

2.3. Scanning electron microscopy

The morphology of nanocomposite membranes was investigated by using Scanning Electron Microscopy (S-4700 Hitachi, Japan). The gold sputtering was carried out on membranes by ion sputtering machine model JFC-1500 JEOL Limited. In order to find the thickness of selective layer of membrane over polysulfone sheet, cross sectional view of membranes were also examined. Liquid nitrogen was used to break membrane for the cross-sectional images.

2.4. X-ray diffraction

The crystallinity of nanocomposite membranes was determined by using STOE X-ray Diffractometer. The scan angle was set to 20–60° at a step size of 0.4° and a step time of 0.5 s/step. The radiation energy used for x-ray diffraction was Cu K α -1 frequency of 1.5406 Å. The method mentioned in literature was used to determine the crystallinity index of casted membranes [39]. The area under the curve of the XRD spectrum between 20 and 60° was considered as total area.

2.5. moisture uptake

The degree of swelling of PVAm/CNC membranes was investigated at room temperature by subjecting them to a humid environment. The membranes were placed in a closed chamber with relative humidity (RH) of 0%. The degree of swelling of membranes was measured by subjecting them to environment with 87% relative humidity. The membranes were placed in such a way that there was no direct contact of membranes with the saturated salt solution. The degree of swelling was calculated after every 24 h on basis of the increase in weight of membranes. The readings were taken for 10 days. Day 1 measurement was taken after 24 h in which membranes were subjected from 0% RH to 87% RH. Equation (1) was used to calculate the degree of swelling [14].

$$DoS (\%) = \frac{S - D}{D} \times 100 \quad (1)$$

where, D is the mass of dry membrane and S is the mass of swelled membranes.

2.6. Permeation test

Permeation testing was conducted to examine the performance of membrane for CO₂ capture. A membrane rig as shown in Fig. 2 was used to conduct permeation testing. The rig has ability to test the membranes at moderately high pressures; up to 20 bars at both humid and dry conditions. Fig. 2 shows the flow diagram of membrane rig.

CO₂ or CH₄ are filled in cylinders which are allowed to flow in feed line, F, controlled by the pressure regulators attached with cylinders. After leaving the cylinder, gas moves towards a two-way valve which provides an option for the gas to be used in dry conditions, F_D, or in humidified conditions, F_H. For dry gas, humidifier, H1, is bypassed. Needle valve NV1 is present, which allows precise control of gas flow. Flow meter, FM1, indicates the flow rate of feed gas before entering to membrane cell. The gas that pass through the membrane, exits the cell from bottom as permeate, P. While that do not pass the membrane, exits from top as retentate, R. Flow rate of permeate is measured manually by bubble flow meter indicated here as FM3.

N₂ is used as the sweep gas. The pressure is controlled and read using pressure regulator and gauge, respectively. Same phenomenon as above takes place in sweep line. Two-way valve, TW2, allows either sweep be humidified, S_H, or dry, S_D. Volume of humidifier is the same as for above. Needle valve, NV2, and flow meter, FM2, controls and measures the flow rate of sweep gas, respectively. However, sweep enters the membrane cell from bottom and exits the permeate line P. The pressure and flow of sweep gas are kept very low. Different membrane compositions were tested for their CO₂ and CH₄ permeability and selectivity. Sweep gas was humidified and then supplied to membranes so that maximum moisture uptake was achieved as indicated by the degree of swelling of membranes. The single gas testing for CO₂ and CH₄ were carried out by supplying the humid gases to the membranes. Effect of pressure was investigated by supplying feed gases at 5, 10 and 15 bar. While, keeping flow rate and temperature constant. The permeability of the gases was measured manually by using a bubble flow meter.

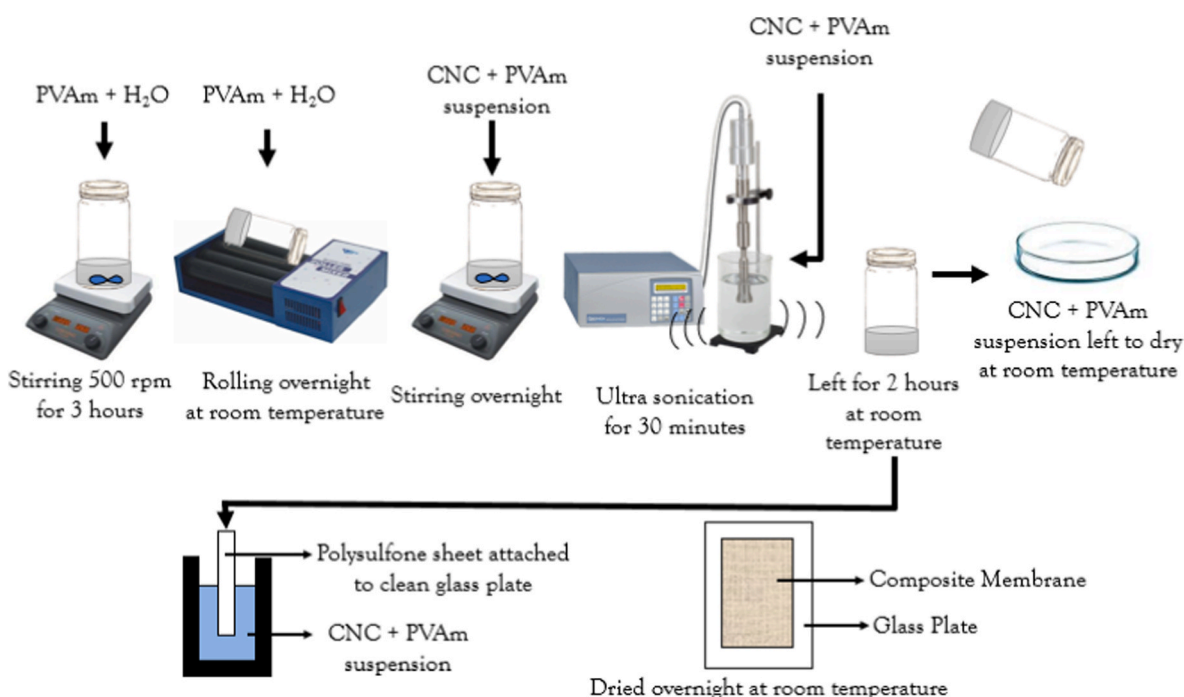


Fig. 1. Cellulose nano-crystals and polyvinyl amine nanocomposite membranes.

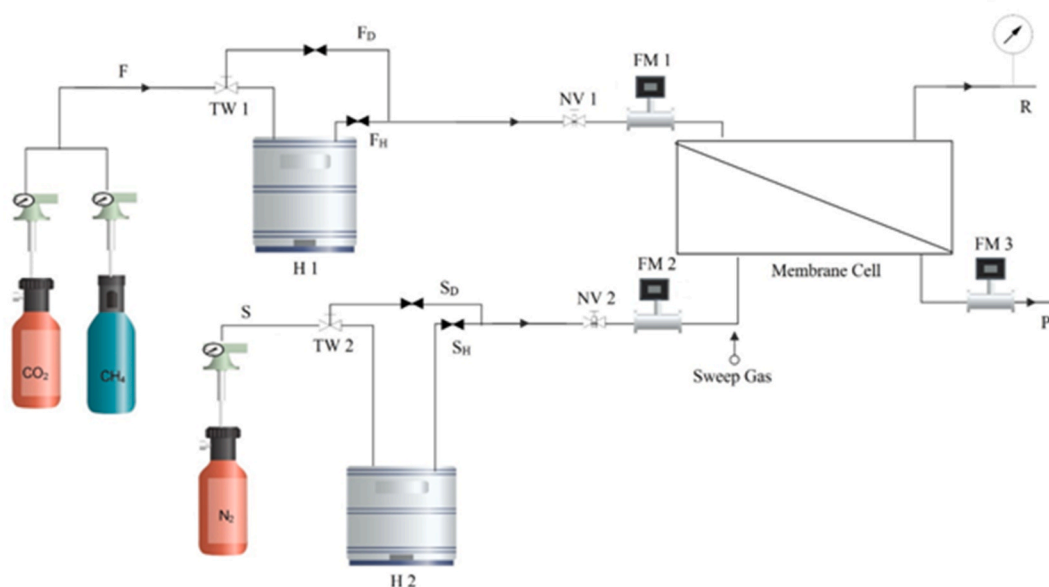


Fig. 2. Flow diagram of gas permeation rig, F = Feed Line, S = Sweep Line, TW = Two Way Valve, F_D = Dry Feed, F_H = Humidified Feed, S_D = Dry Sweep, S_H = Humidified Sweep, H = Humidifier, NV = Needle Valve, FM = Flow Meter, P = Permeate, R = Retentate.

3. Results and discussion

3.1. Characterization

3.1.1. Morphology and thickness of composite membranes

The scanning electron microscopy (SEM) analysis was performed to investigate the morphology and thickness of selective layer. SEM results revealed the smooth and defect free surface of PVAm/1CNC membrane as shown in Fig. 3(a). Furthermore, no agglomeration of nano particles was observed on the membrane surface. This indicates the even dispersion of nano particles within the polymeric matrix. Moreover, no cracks are visible on the membrane surface. Hence, the surface

morphology does not show any adverse effect with addition of CNC. The cross sectional view of PVAm/1CNC composite membrane are represented in Fig. 3(b). Web like structure refers to the micro-porous PSf support with selective PVAm/CNC membrane on the top. Membrane thickness was determined by taking measurements at different parts of the composite membrane. The average thickness observed for PVAm/1CNC membrane was approximately $1.5 \pm 0.12 \mu\text{m}$. Furthermore, the selective layer thickness enhanced with increase in the concentration of CNC in the polymeric membrane as shown in Fig. 3(c). This can be ascribed to the increase in viscosity of the casting solution with increasing the CNC concentration. The addition of 1.5 wt % CNC increases the average thickness of membrane three times of the thickness

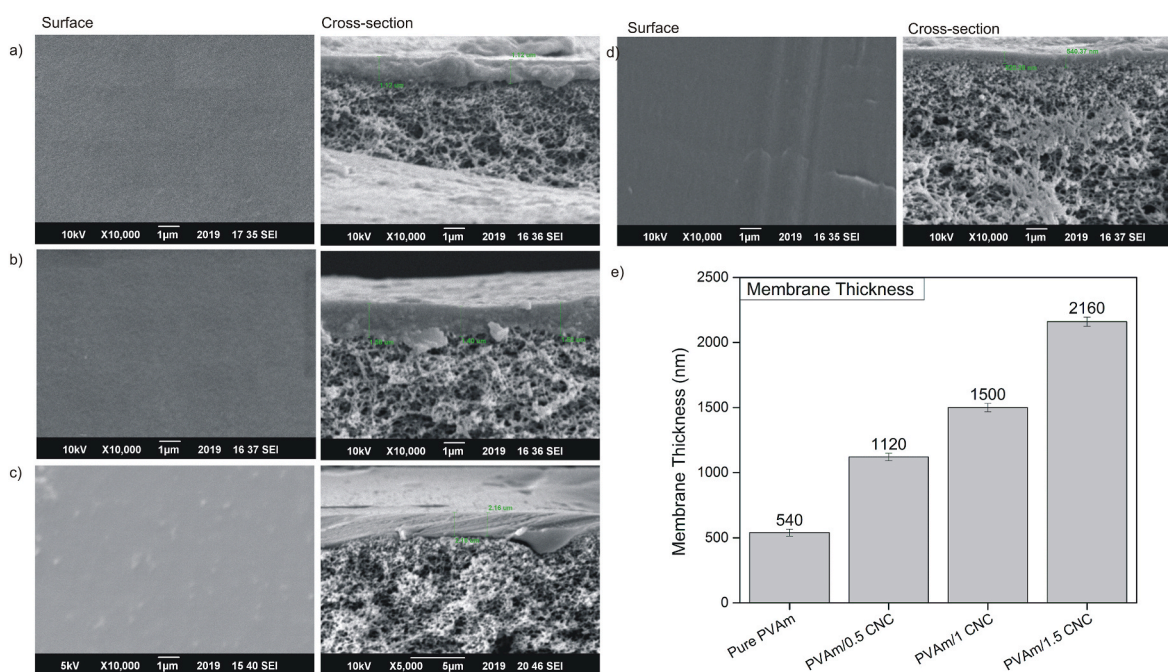


Fig. 3. SEM images of PVAm/CNC membranes with addition of 1 wt% CNC, (a) surface and cross-section morphology of PVAm/0.5CNC, (b) surface and cross-section morphology of PVAm/1CNC, (c) surface and cross-section morphology of PVAm/1.5CNC, (d) surface and cross-section morphology of pure PVAm membrane, and (e) thickness of nanocomposite membranes.

of pure PVAm membrane. However, 1 wt% CNC membrane shows optimized results with thickness of 1500 nm. Hence, an increment in membrane thickness is observed for a successive increase in CNC concentration [40].

3.1.2. Swelling behavior

Degree of swelling of composite membranes was investigated by subjecting them to a RH of 87%. Fig. 4 (a) shows the maximum moisture uptake over a period of 10 days. The maximum swelling was observed until day 5. However, the membrane with 1% CNC concentration absorbed the moisture until day 6. Furthermore, a gradual increase in the degree of swelling was observed for pure PVAm membrane between day 6 and 7. The highest degree of swelling was observed for membrane with 1% CNC concentration i.e. $75.88 \pm 1.1\%$. However, the membrane with 1.5% CNC contents showed a swelling percentage of $68.93 \pm 0.9\%$. The strong reinforcement capability of CNC molecules result in reduced degree of swelling when CNC concentration is increased. This effect resists the mechanical restraining and rejects the further uptake of water molecules resulting in a reduced degree of swelling of PVAm/CNC composite membranes [18]. Increasing CNC concentration imparts strong hydrogen bonding which affixes the polymeric chains thus reducing the moisture uptake capability of membranes [41]. Moreover, reduction in swelling degree can also be correlated with the rise in the crystallinity index of membranes with the increasing CNC concentrations as shown in Fig. 4(b).

3.1.3. Crystallinity of composite membranes

X-ray diffractogram for pure PVAm and PVAm/CNC composite membranes is shown in Fig. 5(a). The crystallinity of all composite membranes was calculated as mentioned in section 2.4. At $2\theta = 21.52^\circ$, a sharp peak appeared in all diffractogram which indicated presence of PVAm. The approximate crystallinity of the pure PVAm membrane was calculated around 42%. No peak shift was observed when CNC was added to PVAm membrane. CNC showed its presence on diffractogram in form of a sharp peak at $2\theta = 23.88^\circ$ [38]. This showed that the addition of CNC increased the crystallinity of composite membranes. Fig. 5(b) showed the effect of CNC concentration on crystallinity. It was observed that increasing the CNC concentration enhanced the crystallinity of composite membranes. Due to highly crystalline nature of CNC, its peak was visible even at low concentrations [42].

PVAm/0.5CNC showed an increased crystallinity as compared to pure PVAm membrane. Maximum crystallinity was attained with addition of 1.5 wt % CNC in nanocomposite membranes i.e. 64.77%. Increasing crystallinity imparts rigidity in polymer and inhibits chain

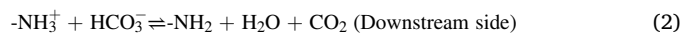
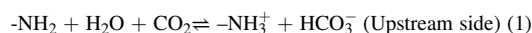
mobility.

3.2. Permeation results

3.2.1. CO₂ and CH₄ permeance and selectivity in effect with CNC concentration

Fig. 6 shows the effect of increasing CNC concentration on membrane performance in terms of permeance and selectivity for CO₂ and CH₄. Addition of CNC had a positive effect on membrane performance for CO₂ separation. It has been observed that permeance and selectivity of CO₂ enhanced with increasing concentration of CNC in PVAm up to the addition of 1 wt% of CNC. From the results as shown in Fig. 6 a & c, it has been observed that the pure PVAm membrane showed permeance of $0.00852 \text{ m}^3(\text{STP})/\text{m}^2 \cdot \text{bar} \cdot \text{hr}$ and selectivity of CO₂/CH₄ around 12 at a pressure of 5 bar. Furthermore, the addition of CNC shows enhanced CO₂ permeance and selectivity for all compositions as compared to pure PVAm. The highest results for CO₂ permeance and CO₂/CH₄ selectivity were obtained by the addition of 1 wt % CNC i.e. $0.0216 \text{ m}^3(\text{STP})/\text{m}^2 \cdot \text{bar} \cdot \text{hr}$ and 41, respectively at 5 bar. However, the decreasing trend has been observed for permeance of CH₄ with increasing CNC concentration. For PVAm/1CNC composite membrane, CH₄ permeance was observed to be $0.000526 \text{ m}^3(\text{STP})/\text{m}^2 \cdot \text{bar} \cdot \text{hr}$ at 5 bar.

In addition to membrane structure, the properties of gas pair to be separated is also very important for the performance of membrane. In case of novel composite membranes casted in this work, the separation layer includes polymer phase, dispersed nano filler phase and interaction of these two. In PVAm/CNC composite membranes, the CH₄ is transported only by solution diffusion mechanism. Whereas, in addition to solution diffusion mechanism CO₂ is dominantly transported by facilitated transport mechanism. Addition of CNC in PVAm matrix enhanced the moisture uptake capability of composite membrane. That results in the increased rate of facilitated transport of CO₂. CO₂ is a water soluble gas; therefore, the presence of high water contents increased CO₂ transport in form of bicarbonate ions. Furthermore, the presence of amine groups on backbone of polymeric chain act as fixed carries and selectively transport CO₂ through the membrane. The chemical equation for the reactions occurring in membrane is defined by the following reactions [10]:



The addition of CNC in PVAm provides non selective and less resistant pathways for gas transportation. The moisture uptake induces

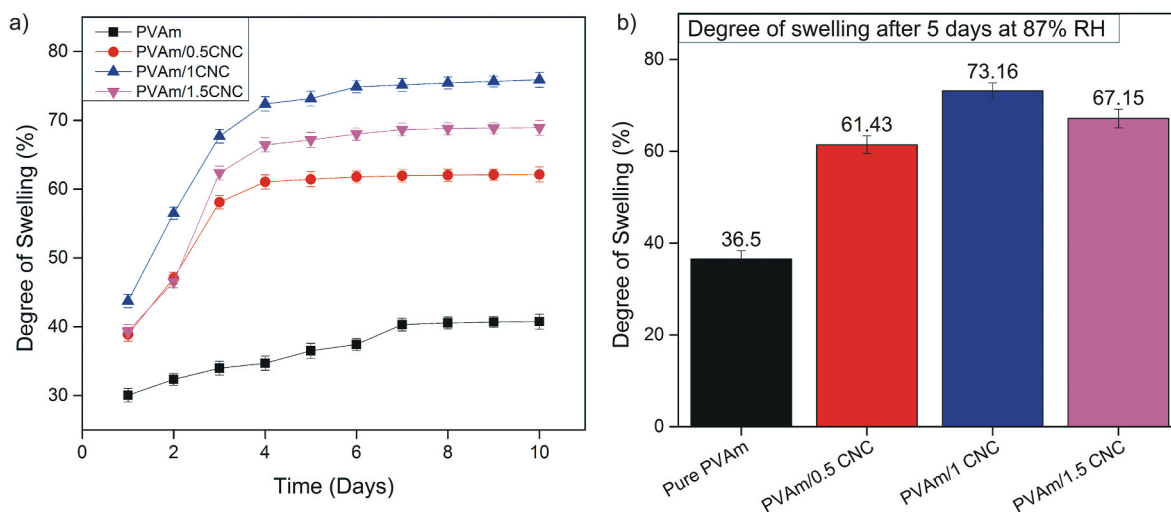


Fig. 4. Degree of swelling for ten days (a) degree of swelling of PVAm/CNC membranes compared with pure PVAm membrane at 87% RH (b) maximum degree of swelling after 6 days at 87% RH.

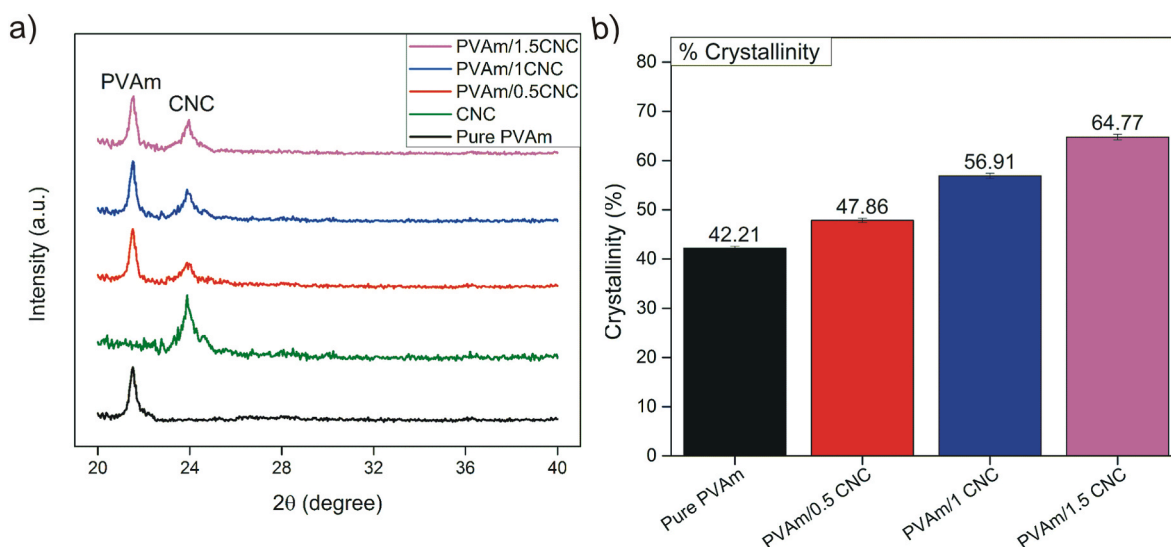


Fig. 5. XRD analysis of composite membranes, a) pure PVAm and PVAm/CNC membranes, b) Effect of CNC concentration on % age crystallinity.

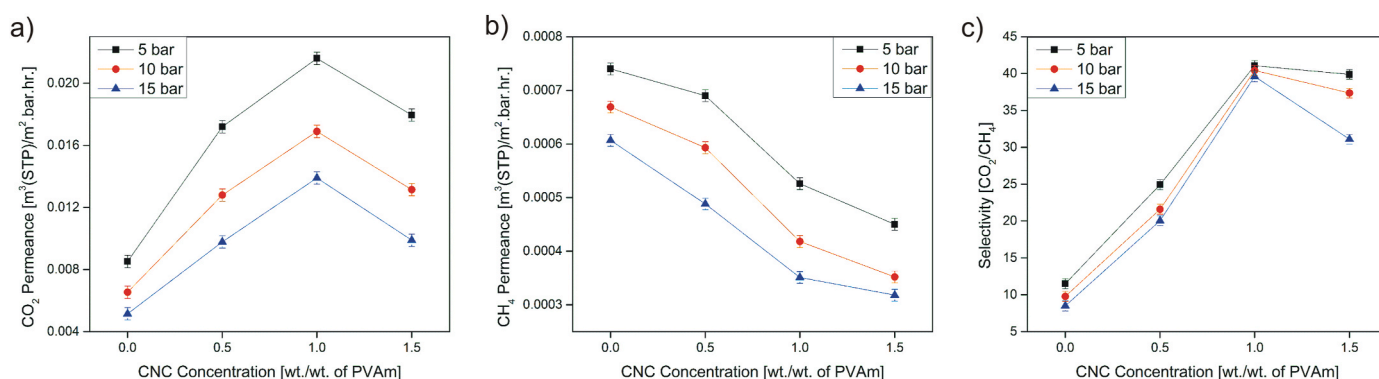


Fig. 6. Effect of increasing CNC concentration on permeation performance of PVAm/CNC membranes (a) CO₂ permeance for pure PVAm and PVAm/CNC membranes (b) CH₄ permeance for pure PVAm and PVAm/CNC membranes and (c) Selectivity of CO₂/CH₄ for pure PVAm and PVAm/CNC membranes.

swelling behavior which increases free volume in between the polymeric chains and also increases the chain flexibility. This increases the diffusive transport of gases across the membrane. As the kinetic diameter of CO₂ and CH₄ are 3.3 Å and 3.8 Å, respectively. So, both gases can selectively pass through swelled areas [43]. Even though, the permeance of CO₂ is much higher as compared to CH₄. This can be attributed to the high solubility of CO₂ in water.

Furthermore, it has been observed that the value of permeance for both CO₂ and CH₄ has reduced after addition of CNC above 1 wt%. The decline in membrane performance above 1 wt% CNC can be attributed towards the reduced moisture content and increased crystallinity. Increased crystallinity not only induces rigidity in polymer matrix but also reduced moisture uptake ability of composite membranes as explained in section 3.1.3. Therefore, transportation of gas by solution diffusion mechanism has declined. Furthermore, as explained in section 3.3.2 that increasing CNC concentration in PVAm significantly enhanced the selective layer thickness beyond addition of 1 wt% CNC. Hence, it has also contributed to reduce gas permeation through the membrane. The CH₄ permeates only by solution diffusion mechanism due to its non-reactive nature. Hence, its permeance showed sharper decline with increase in chain rigidity. However, the decrease in moisture uptake ability dominantly affects the transport of CO₂ as it is a water soluble gas and mainly transported through facilitated transport [21]. The transportation mechanism for both the gases is represented in Fig. 7. It can be seen that CO₂ is transported by i) reaction with amine carriers present on

backbone of polymer matrix. However, due to limited carrier concentration, there will be no further increase in rate of CO₂ transport once a saturation state occurs. This is intrinsic property of PVAm membranes. Addition of CNC had no effect on this property. ii) Transportation of CO₂ as bicarbonate ions aids by the presence of moisture contents. Addition of CNC plays significant role in this transport as it enhanced the

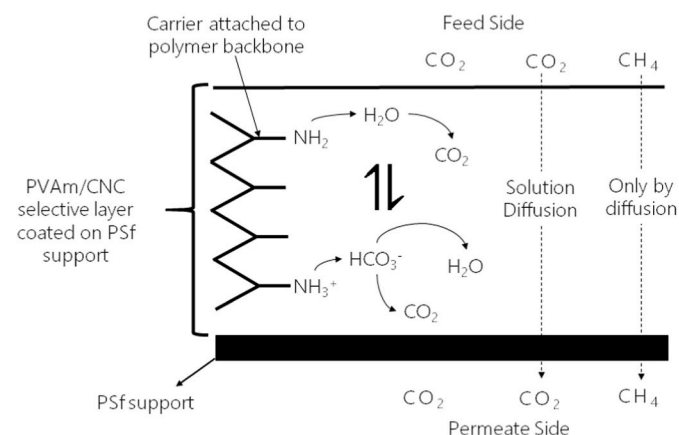


Fig. 7. Mechanism of gas transport through PVAm/CNC nano-composite membranes.

moisture uptake ability of membrane, and iii) Transport of CO₂ by molecular diffusion. Whereas, the only transport mechanism is molecular diffusion for CH₄. Therefore, addition of 1 wt% CNC showed positive effects on CO₂ transport but does not enhance the membrane performance for CH₄ transport.

3.2.2. Effect of feed pressure on gas permeance of composite membranes

The pure PVAm and PVAm/CNC composite membranes were tested at a pressure of 5, 10 and 15 bar for CO₂ and CH₄ permeance. It was observed that permeance of both gases and selectivity of CO₂/CH₄ decreased as a result of increasing pressure for all the formulated membranes. The highest CO₂ permeance and CO₂/CH₄ selectivity was achieved by PVAm/1CNC membrane at 5 bar pressure i.e. 0.0216 m³(STP)/m².bar.hr. and 41, respectively as shown in Fig. 8 (a & c). However, addition of 1 wt % CNC showed decline in permeance of CH₄ using pure PVAm membrane at 5 bar. The values of CH₄ permeance for PVAm and PVAm/1CNC membranes are 0.00074 m³(STP)/m².bar.hr. and 0.000526 m³(STP)/m².bar.hr., respectively. Furthermore, the drop in permeance for CO₂ is rapid in the beginning with increasing pressure. This behavior is attributed to the saturation state of all amine carriers present on polymer matrix. Once the carriers become saturated in pure PVAm membrane, CO₂ is transported only by solution diffusion mechanism. However, the dominating phenomenon is still facilitated transport in PVAm/CNC membranes with aid of moisture content present in membranes. Hence, the values of CO₂ permeance and selectivity of all CNC containing membranes are higher than pure PVAm membranes at all pressure.

Performance of water swollen membranes was high when the feed gas was fully humidified at low pressure. Increased feed pressure enhances the flow of gas. Further high pressure squeezes the membrane and increase the flow of moisture content through the membrane. Hence, moisture contents in the membrane get decreased even at high % RH [17]. Reduction of moisture contents, decrease the facilitated transport of CO₂ across the membrane [12]. Furthermore, at the high feed pressure plasticization occurs in polymeric membranes that reduces the chain mobility and impart rigidity in membrane structure. This further reduced membrane performance at high pressures [18]. In addition, the high feed pressures introduce compression on polymer matrix that reduces the free voids available for solution diffusion of gases. Hence, results in the decline of permeance of both CO₂ and CH₄. Thus, the decrease in CO₂/CH₄ selectivity was not very prominent except for PVAm/1.5CNC membrane. The selectivity dropped from 40 to 31 when feed pressure was increased from 5 to 15 bar as shown in Fig. 8 (c). PVAm/1CNC showed a very minute selectivity drop i.e. 41 to 39, with increase in pressure from 5 to 15 bar.

3.2.3. Effect of relative humidity on facilitated transport of CO₂

PVAm/1CNC membranes were investigated for the effect of RH on transport of CO₂ and CH₄ at 5 bar pressure as shown in Fig. 9. The effect of %RH was investigated by subjecting the membranes to different

humidity levels of 0, 25, 50, 75 and 100% before testing. The different humidity levels were achieved by data obtained from the degree of swelling graphs. Results showed that increasing %RH improved the CO₂ permeance and selectivity. This is due to the fact that higher moisture contents increases facilitated transport of CO₂ across the membrane [40]. Furthermore, an increase in %RH enhances the degree of swelling. Hence, open the amorphous pores in polymer matrix providing non selective bypass for diffusion of CO₂ and CH₄ molecules. However, CO₂ moves across the membrane by facilitated and diffusive transport but CH₄ only passes through by diffusive transport. Hence, the increase in CH₄ permeance is very low with a rise in %RH as compare to CO₂ permeance [44]. At 0% RH, CO₂ and CH₄ showed a permeance of 0.00279 m³(STP)/m².bar.hr. and 0.000472 m³(STP)/m².bar.hr., respectively. Increasing the %RH to 100%, CO₂ permeance enhanced approximately 10 folds. While, CH₄ permeance just increased to 0.000526 m³(STP)/m².bar.hr. The rise in the %RH from 0 to 100%, increased the selectivity of membrane from 6 to 41, respectively. High selectivity rise can be attributed to the increase in permeance of CO₂ with rising %RH.

4. Conclusions

PVAm/CNC membranes were successfully fabricated and tested for the effect of CNC concentration and feed pressure on separation performance of CO₂ and CH₄. Addition of CNC has improved the permeance and selectivity of PVAm membrane for CO₂ transport. However, addition of CNC does not showed any significant change on CH₄ permeance. As compared to pure PVAm membrane, enhanced separation performance was observed when CNC was added in membranes. Furthermore, addition of CNC enhanced the moisture uptake of formulated membranes. The moisture uptake was increased up to the addition of 1 wt% CNC and started decreasing beyond this concentration. PVAm/1CNC showed a swelling degree of 75.88 ± 1.1%. However, the thickness of selective layer and crystallinity of PVAm/CNC membranes showed increasing trend with increasing CNC concentration. In addition, it was found that by increasing feed pressure the permeance of both gases for the casted membranes declined. However, this decline was more prominent for CH₄ gas. Furthermore, it is highly recommended to work at maximum swollen conditions to get maximum benefit of facilitated transport of CO₂. It was seen that PVAm/1CNC membrane showed the highest CO₂ permeance and selectivity of 0.0216 m³(STP)/m².bar.hr. and 41, respectively at a pressure of 5 bar. According to the results, 1 wt % CNC was optimized concentration and at 5 bar pressure, membrane showed best results.

Author Statement

Farooq sher and Zaib Jahan conceptualized the project. Uzair Saeed and M. Bilal Khan Niazi performed investigation and formal analysis. Erum Pervaiz did the project administration. Uzair Saeed, Zaib Jahan and M. Bilal Khan Niazi wrote the original draft.

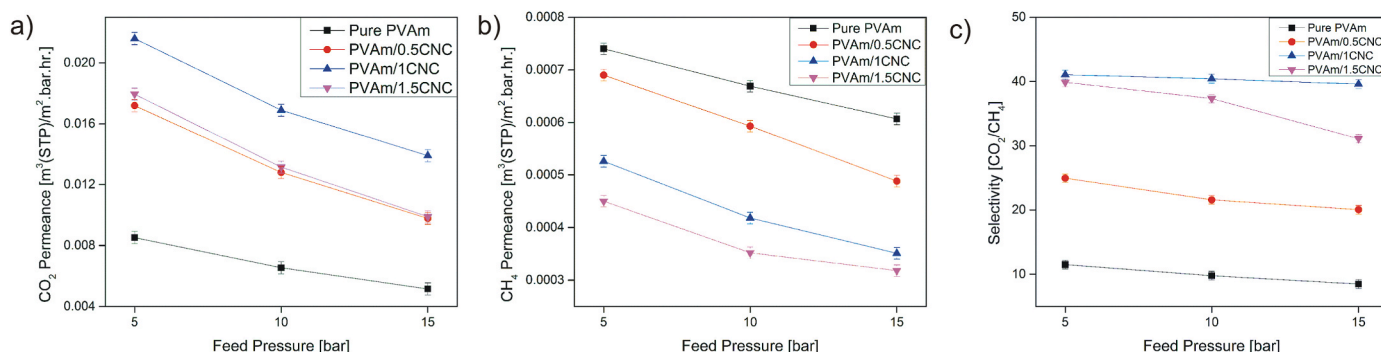


Fig. 8. Effect of feed pressure on (a) CO₂ permeance (b) CH₄ permeance (c) Selectivity CO₂/CH₄.

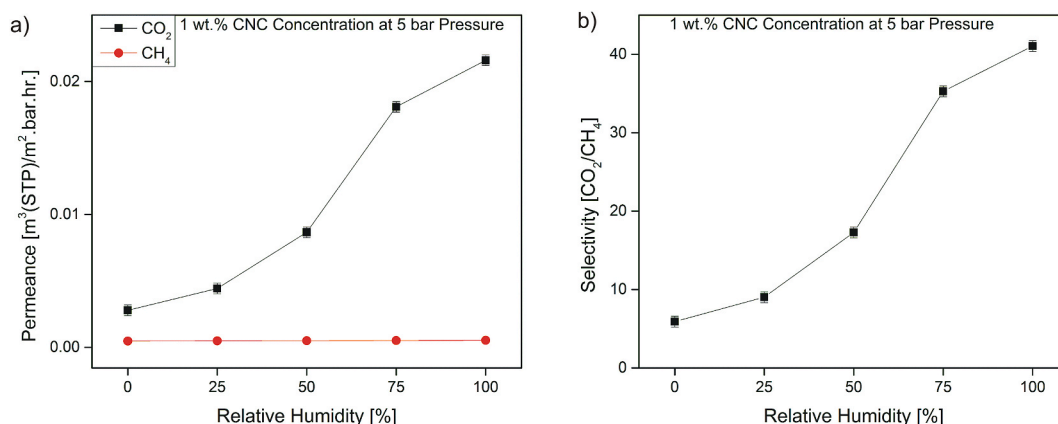


Fig. 9. Percentage RH effect on facilitated transport (a) CO_2 and CH_4 permeance (b) CO_2/CH_4 selectivity.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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